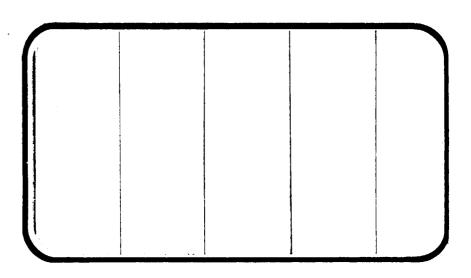


NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

NASA CR-

141535



N75-24817

PESULTS OF DYNAMIC (NASA-CF-141535) STABILITY TESTS CONDUCTED OF A .012 SCALE MODEL MODIFIED 089 B SHUTTLE OPRITER IN THE AEDC-VKF TUNNEL B AT & MACH NUMBER OF 8.0 (LA42) (Chrysler Corp.) 39 p HC \$3.75

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SPACE SHUTTLE

AEROTHERMODYNAMIC DATA REPORT



JOHNSON SPACE CENTER

HOUSTON, TEXAS

DATA MANagement services



DMS-DR-2132 NASA CR-141,535

RESULTS OF DYNAMIC STABILITY TESTS

CONDUCTED ON A .012 SCALE MODEL MODIFIED

089 B SHUTTLE ORBITER IN THE AEDC-VKF TUNNEL B

AT A MACH NUMBER OF 8.0 (LA42)

Prepared Under NASA Contract Number NAS9-13247

by

Data Management Services Chrysler Corporation Space Division New Orleans, La. 70189

for

Engineering Analysis Division

Johnson Space Center National Aeronautics and Space Administration Houston, Texas WIND TUNNEL TEST SPECIFICS:

Test Number: AEDC V41B-48A

NASA Series Number: LA42

Model Number: LaRC Modified 089B Orbiter Test Dates: June 25 and July 27, 1974

Occupancy Hours: 20

FACILITY COORDINATOR:

Larry Trimmer

ARO, Inc. von Karman Gas Dyn. Facility

Arnold Engineering Development Center

Air Force Systems Command

Arnold Air Force Station, Tennessee 37389

Phone: (615) 455-2611 Ext. 7377

PROJECT ENGINEER:

NASA Cognizant Engineer:

Bob L. Uselton Delma C. Freeman, Jr.

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Data Management Services Flight Technology Branch

Chrysler Corporation Space Division assumes no responsibility for the data presented other than display characteristics. RESULTS OF DYNAMIC STABILITY TESTS

CONDUCTED ON A .012 SCALE MODEL MODIFIED

089 B SHUTTLE ORBITER IN THE AEDC-VKF TUNNEL B

AT A MACH NUMBER OF 8.0 (LA42)

ABSTRACT

Experimental aerodynamic investigations were conducted during June and July 1974 on a .012 scale model of a NASA/Langley modified version of the Rockwell 089B Space Shuttle Orbiter. The modification consisted of using the 139B orbiter nose forward of station 500 on the 089B fuselage. Using the forced oscillation test technique, dynamic stability derivatives were measured in the pitch, yaw and roll planes at a Mach number of 8 over an angle of attack range from -4° to 28°. Plotted and tabulated results are presented herein.

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5	Effect of Reynolds Number on Dynamic Stability in Roll	В	2
6	Effect of Vertical Tail on Dynamic Stability in Yaw	С	3
7	Effect of Vertical Tail on Dynamic Stability in Roll (RN = 2.34)	В	4
8	Effect of Vertical Tail on Dynamic Stability in Roll (RN = 4.72)	В	5

Schedule of Coefficients Plotted:

- A) CLMALF, CLMQ vs ALPHA
- B) CBLBTA, CBLP vs ALPHA
- C) CYNBTA, CYNR vs ALPHA

NOMENCLATURE

SYMBOL	PLOT SYMBOL	DEFINITION
Ь	BREF	reference length for lateral coefficients, (wing span) inches
$(C_{\lambda_{2}} \sin \alpha)$	CBLBTA	$\partial C_k/\partial eta$, per radian
$(C_{\lambda_{\mathbf{p}}} + C_{\lambda_{\mathbf{B}}})$ since) CBLP	roll-damping coefficient, $\partial C_{\ell}/\partial$ (pb/2V.) + $\partial C_{\ell}/\partial$ ($\dot{\beta}$ b/2 V) sin α , per radian
C_{m}	CLM	pitching moment coefficient
$c_{m_{\alpha}}$	CLMALF	slope of pitching-moment vs angle of attack curve, per radian
$(C_{m_q} + C_{m_{\dot{\alpha}}})$	CLMQ	damping_in-pitch derivatives, $\partial C_m/\partial (qc/2V_p) + \partial C_m/\partial (\dot{qc}/2V_p)$, per radian
c_n	CYN	yawing moment coefficient
$c_{\mathbf{n}_{\mathcal{A}}}$	CYNBTA	slope of yawing moment vs angle of sideslip curve, per radian
$(C_{np} + C_n) \sin \alpha$) CYNP	yawing moment coefficient due to roll rate $(C_n/+(pb/2V_{})+\partial C_n/\partial (\beta b/2V_{o})\sin\alpha, \ \text{per radian}$
$(C_{n_r}-C_{n_3})$	CYNR	damping-in-yaw derivative, $\sigma C_n/\sigma (r_b/2V_*) = \sigma C_n/\sigma (r_b/2V_*)$, per radian
č	LREF	reference length for longitudinal coefficients (wing mean aerodynamic chord) inches
p	-	roll velocity, radians/see
q		pitch velocity, radian/sec
q	Q(PSF)	freestream dynamic pressure, psf
r		yaw velocity, radians/sec
R _N	RN	Reynolds number based on model length
SREF	SREF	reference area, (wing planform area) ft^2
V ,	-	freestream velocity, ft/sec

NOMENCLATURE (Concluded)

SYMBOL	PLOT SYMBOL	DEFINITION	
X _{c.g.}	XMRP	longitudinal location of pivot axis	s
Y _{c.g.}	YMRP	lateral (moment reference point (theoretical c.g.)	
Z _{c.g.}	ZMRP	vertical	
α	ALPHA	angle of attack, degrees	
β	BETA	angle of sideslip, degrees	

NOTE: dot over symbol (i.e., $\dot{\alpha}$) denotes time rate of change of the symbol.

CONFIGURATIONS INVESTIGATED

An 0.012 scale model of the Rockwell 089 B orbiter modified forward of fuselage station 500 to the 139 B orbiter configuration was tested with and without the vertical tail in the yaw and roll modes and in the full configuration only in the pitch mode. Figure 2 depicts the configuration tested which included the OMS pods but not the body flap. Table I gives the tunnel conditions existing during the test while Table II delineates the configurations investigated at specific conditions.

Table III lists pertinent dimensional information about each model component tested.

TEST MECHANISM

PITCH/YAW

The pitch/yaw damping test mechanism (Reference 1) utilizes a cross flexure pivot, an electric shaker motor and a one-component moment beam which is instrumented with strain gages to measure the forcing moment of the shaker motor, Figure 3a. The motor is coupled to the moment beam by means of a connecting rod and flexural linkage which converts the translational force to a moment (70 in.-lb maximum) to oscillate the model at amplitudes up to ± 3 deg (depending on flexure balance) and frequencies from 2 to 20 Hz. The cross flexures, which are instrumented to measure the pitch/yaw displacement, support the model loads and provide the restoring moment to cancel the inertia moment when the system is operating at its natural frequency. Presently, two cross flexure balances exist and each is composed of three beams with single unit construction. The beam thickness for each balance is 0.087 and 0.17 in. and the restoring moment produced by each balance is -132 and -938 ft-lb/radian, respectively. Since the moment beam which is used to measure the forcing moment is not subjected to the static loads, it can be made as sensitive as required for the dynamic measurements. Beams exist which can measure up to ± 0.6 , ± 3 , ± 11 , ± 25 , and ± 70 in.-1b. A pneumatic- and springoperated locking device is provided to hold the model during injection into or retraction from the tunnel or during tunnel starts. The crossflexure balances can be supported by an elliptical cross-section sting

(provides support strength and maximum model clearance but is not water-cooled) or a 1.75-in.-dia. water-cooled sting (normally used with the roll-damping balance, Reference 2). The water-cooled sting was used during the present tests in conjunction with the -132 ft-lb/radian cross-flexure balance and primarily the +3 in.-lb. moment beam.

ROLL

The roll-damping test mechanism (Reference 2) utilizes a waterjacketed, five-component balance, twin beam flexures, roller bearings to
support the loads, and electric printed-circuit drive motors, Figures 3b
and 3c. The motors are directly coupled to the balance and supply up to
120 in.-lb roll moment to oscillate the system at amplitudes up to ±3 deg
and at frequencies from 2 to 20 Hz. The twin beam flexures mount from
the stationary sting to the oscillating water jacket and provide a
restoring moment which cancels the inertia moment when the system is
operating at the natural frequency of the model-flexure system. The
flexures are instrumented to measure the roll displacement. The entire
mechanism is water-cooled to permit testing in the hypersonic tunnels.

Two five-component balances have been fabricated for the system to provide good balance sensitivity over the load range. Both balances utilize outrigger beams in the yaw sections and thin-ribbed flexures in the roll section to provide sensitive yaw and roll outputs while maintaining large normal-force capacity and rigidity in yaw. Semiconductor gages are also utilized for the yaw and roll sections for additional sensitivity. The -59 balance was used during the present test.

TEST INSTRUMENTATION

The forced oscillation instrumentation (Reference 1 and 2) utilizes an electronic analog system with precision electronics. The control, monitor, and data acquisition instrumentation is contained in a portable console that can be easily interfaced with the instrumentation of the various wind tunnels.

The control instrumentation provides a system which can vary the oscillation frequency, oscillation amplitude, and angular position of the model within the flexure limits (for both pitch, yaw and roll tests). The oscillation amplitude is controlled by an electronic feedback loop which permits testing both dynamically stable and unstable configurations.

Data are normally obtained at or near the natural frequency of the model-flexure system; however, the electronic resolvers used permit data to be obtained off resonance. The gages or the balances are excited by d-c voltages, and outputs are increased to optimum values by d-c amplifiers. Typical balance outputs from an oscillating model are composed of oscillatory components (OC) superimposed on static components (SC). These components are separated in the data system by bandpass and lowpass filters. The SC outputs are sent directly to the tunnel scanner and computer, which for the pitch/yaw tests calculate the static moment coefficients and sting deflections and for the roll test calculate the static-force and moment coefficients. The OC outputs are input to the resolver instrumentation and the precise frequency-measuring instrument which were

developed at VKF. The resolvers utilize very accurate analog electronic devices to process the OC signals and output d-c voltages, which for the pitch/yaw tests are proportional to the amplitude squared, the in-phase and quadrature b lance components, and the in-phase and quadrature sting components and for the roll tests are proportional to the amplitude squared, the in-phase and quadrature (90 deg out of phase) moments, and the quadrature vawing moments. A switch is also provided in the resolver system to bypass the phase shift network so that the in-phase yawing moments can be determined during the roll tests. The resolver and frequency outputs are read by the tunnel scanner and sent to the computer. The frequency instrument controls the length of the data interval in increments from approximately 2 to 60 seconds, during which time the scanner reads each input approximately 10 times per second. The average values of the readings are calculated by the computer, which then uses these average values to calculate the dynamic coefficients.

 $\int J$

TEST FACILITY DESCRIPTION

The AEDC-VKF Tunnel B is a continuous, closed-circuit, variable density wind tunnel with an axisymmetric countoured nozzle and a 50-in. diameter test section. The tunnel can be operated at a nominal Mach number of 6 or 8 at stagnation pressures from 20 to 300 and 50 to 900 psia, respectively, at stagnation temperatures up to 1350°R. The model may be injected into the tunnel for a test run and then retracted for model cooling or model changes without interrupting the tunnel flow. A description of the tunnel may be found in Reference 3. A tunnel depiction is given in Figure 3d.

REFERENCES

- 1. Burt, G.E. "A Description of a Pitch/Yaw Dynamic Stability Forced-Oscillation Test Mechanism for Testing Lifting Configurations", AEDC-TR-73-60.
- 2. Burt, G. E. "A Description of a Forced-Oscillation Test

 Mechanism for Measuring Dynamic-Stability Derivatives in

 Roll", AEDC-TR-73-49.
- Test Facilities Handbook (Tenth Edition) von Karman Gas
 Dynamics Facility, Volume 3, AEDC, May 1974.

TABLE I

TEST : AEDC V 41 B	- 48 A		DATE : 7/28/74
	TEST CO	ONDITIONS	
	25/4/24/25 24/4/25	T	
MACH NUMBER	REYNOLDS NUMBER	STAGNATION PRESSUR (pounds/sq. inch)	RESTAGNATION TEMPERATURE (degrees Rankine)
8,0	1.18	200	850
8.0	2.36	400	850
8.0	4.75	850	886
			
	:		

	· · · · · · · · · · · · · · · · · · ·		
	Con Tout /Tost M	lo chamiem)	
BALANCE UTILIZED:	See Text (Test M	lechan (Siii)	
	CAPACITY:	ACCURACY:	COEFFICIENT TOLERANCE:
NF			
SF			
AF	4.		
PM			
RM			
YM	<u></u>		
COMMENTS			,
COMMENTS:			

CONTINUES CONT	TEST: AERC	TEST : AEDC 1/418-4/84 (14-42)		DATA SE	T.'RUN N	UMBER (SET/RUN NUMBER COLLATION SUMMARY	SUMMARY	DAIL	K_/01/01	7	
0 8 KEL 1 1 1 1 1 1 1 1 1	EINTA SET		SCMD.			PARAME	FERS/VALUES		Ž		UMBERS	
	ICENTIFIEP	, workenson	\vdash	RE,					RUR	8.	G	
A 0 236 A 0 237 A 0 237 A 0 472 A 0 472 A 0 474 A 0 0 474 A 0 0 474 A 0 0 474 A 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		3WV		1.18						-		
A 0 482 3 4			-	2.3						2		
A 0 257 A 0 2.34 A 0 4.72 A 0 4.74 A 0 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	60			8 7	-6					3		
A 0 2.57												
A 0 2.57 A 0 4.72 A 0 4.72 A 0 4.74 A 0 1.34 A 0 1.	1	SWV	 	2.3						7		
A 0 2.35 A 0 4.72 A 0 4.72 A 0 4.74 A 0 6.74 A 0 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	l	3W		2.5						5		
A 0 2.35 A 0 2.34 A 0	:											-3
A 0 2.35		W.V.		1.19						3		1
A O 4.72			-	2.3						2		NO
A O 4.74	03			4.7						•		100
M ₃ 25 81 37 43 49 55 61 67 MA ACH 10 VAR 21 10 VAR	Ĺ	3W	-	2.3						7		13
M ₃ 25 31 37 43 49 55 61 67 67 67 67 67 67 67 67 67 67 67 67 67	1 05	•		4.7						00		
M ₉ 25 31 37 43 49 55 61 67 CYP. CYP. CYP. CYP. CYP. CYP. CYP. CYP.												
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M ₉ 25 31 37 43 49 55 61 67 ALPHA CYP. CH. GLM							·					T
M ₉ 25 31 37 43 49 55 61 67 67 67 67 67 67 67 67 67 67 67 67 67				\dashv								
M3 25 61 67 67 19 55 61 67 67 64 67 67 67 61 67 67 61 67 67 61 67 67 61 67 61 67 61 67 61 67 61 67 61 67 61 61 61 61 61 61 61 61 61 61 61 61 61												
CYP. CH. GLM . CY	CLME, C	LMALF , CYNBRIA			ءَ [-	5	55	61	67	75.76
Ar-3-25 AK+2. COEFFICENTS RE-3-25	CBLP, RB				G+M	, '57'	, CY.	, 4.95	CYMR	MACH	449.4A	11.0
Ac - 20- 70	•	A: -3 -> 24	•		COEF	FICENTS				IDVAR (1)	10VAR (2)	20 2
							ı					

TABLE III.

MODEL DIMENSIONAL DATA

MODEL COMPONENT : BODY - 089B-139B (Modified Nose)	
GENERAL DESCRIPTION Nose section fr	om full-scale s	tation 238.0 to
STA. 500 from NAR drawing VL70-000139B.	Remaining bod	y AFT of STA_500
from NAR drawing VL70-000093.		
DRAWING NUMBER:	3	
DIMENSIONS: (inches)	FULL SCALE	.012 MODEL SCALE
Length	1290.3	15.484
Max Width	265.0	3.180
Max Depth	248.0	2.976
Fineness Ratio	4.869	4.869
Area		
Max. Cross—Sectional (ft ²)	456.40	.0657
Planform		
Wetted		
Base		

TABLE III. (CONTINUED)

MODEL COMPONENT: ELEVON		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
GENERAL DESCRIPTION: CONFIGURATION PER LINES DATA FOR (1) OF (2) SIDES	VL70-000093	
DATA FOR (1) OF (2) SIDES	<u> </u>	
MODEL SCALE = 0.012		
DRAWING NUMBER: VL70-000093		
DIMENSIONS: (inches)	FULL-SCALE	.012 MODEL SCALE
Area (ft ²)	205.517	.02959
Span (equivalent)	353.34	4.24
Inb'd equivalent chord	114.78	1.377
Outb'd equivalent chord	55.00	66
Ratio movable surface chord/ total surface chord		
At Inb'd equiv. chord	.208	.208
At Outb'd equiv. chord	.400	.400
Sweep Back Angles, degrees		
Leading Edge	0.00	0.00
Tailing Edge	-10. 02	-10.02
Hingeline	0.00	0.00
Area Moment (Normal to hinge line)-Ft3	1548.07	.00267

TABLE III. (CONTINUED)

MODEL COMPONENT: RUDDER		
GENERAL DESCRIPTION: CONFIGURATION PER LINE	S VL 70-000095	
SCALE MODEL = .012		
DRAWING NUMBER: VL70-000095		
DIMENSIONS: (inches)	FULL-SCALE	.012 MODEL SCALE
Area (ft ²)	106.38	.0153
Span (equivalent)	201.0	2.412
Inb'd equivalent chord	91.585	1.099
Outb'd equivalent chord	50.833	0.610
Ratio movable surface chord/ total surface chord		
At Inb'd equiv. chord	0.400	0.400
At Outb'd equiv. chord	0.400	0.400
Sweep Back Angles, degrees		
Leading Edge	34.83	34.83
Tailing Edge	26.25	26.25
Hingeline	34.83	34.83
Area Moment (Normal to hinge line)-Ft3	526.125	.00091

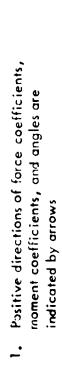
TABLE III. (CONTINUED)

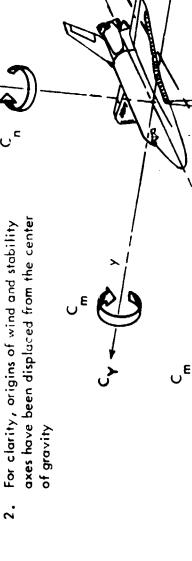
MODEL COMPONENT: Vertical Tail		
GENERAL DESCRIPTION: Centerline vertical ta	il double wedge a	irfoil with
rounded leading edge.		
Scale Model = .012		
DRAWING NUMBER: VL70-000095		
DIMENSIONS: (inches)	FULL-SCALE	.012 MODEL SCALE
Area (theo) ft. ²	413.25	.0595
Span (equivalent)	315.72	3.789
Inb'd equivalent chord	268.50	3.222
Outb'd equivalent chord	108.47	1.302
Ratio movable surface chord/ total surface chord		
At Inb'd equiv. chord		
At Outb'd equiv. chord		
Sweep Back Angles, degrees		
Leading Edge	45	45
Tailing Edge	26.249	26.249
Hingeline		
Area Moment (Normal to hinge line)		

TABLE III. (CONCLUDED)

MODEL COMPONENT: WING		
GENERAL DESCRIPTION: Orbiter Configuration per	r Lines VL70-0000	93
NOTE: (Dihedral angle is defined at the lower	surface of the w	ing at the 75.33%
element line projected into a plane per	rpendicular to the	e FRL).
SCALE MODEL - 0.012		
DRAWING NUMBER: VL70-000093		.012
DIMENSIONS: (inches)	FULL-SCALE	MODEL SCALE
TOTAL DATA		
Area (ft ²) Planform Wetted Span (equivalent) Aspect Ratio Rate of Taper Taper Ratio Diehedral Angle, degrees Incidence Angle, degrees Aerodynamic Twist, degrees Toe-In Angle Cant Angle Sweep Back Angles, degrees Leading Edge Trailing Edge Trailing Edge O.25 Element Line Chords: Root (Wing Sta. 0.0) Tip, (equivalent) MAC, inches Fus. Sta. of .25 MAC W.P. of .25 MAC	2690.00 936.68 2.265 1.177 0.200 3.500 3.000 +3.000 -10.24 35.209 689.24 137.85 474.81 1136.89 299.20	.3874 11.24 2.265 1.177 0.200 3.500 3.000 +3.000 -10.24 35.209 8.271 1.654 5.698 13.643 3.590
Airfoil Section Root	دستب ق روست کی در کسی	
Tip EXPOSED DATA		
Area _(ft) Span, (equivalent) Aspect Ratio Taper Ratio Chords	1752.29 720.68 2.058 0.2451	2523 8.648 2.058 0.2451
Root Tip MAC Fus. Sta. of .25 MAC W.P. of .25 MAC B.L. of .25 MAC		6.749 1.654 4.716 14.224 3.602
D.L. OI .23 MAG	143.76	1.725

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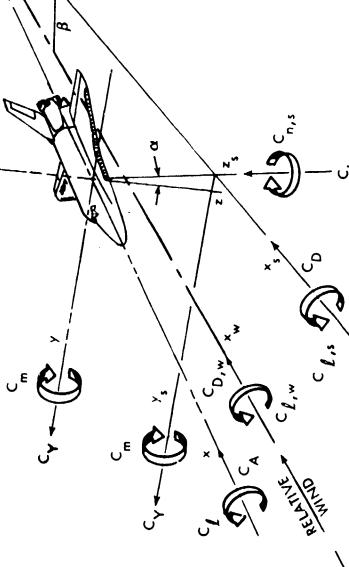


Figure 1. Axis System

4

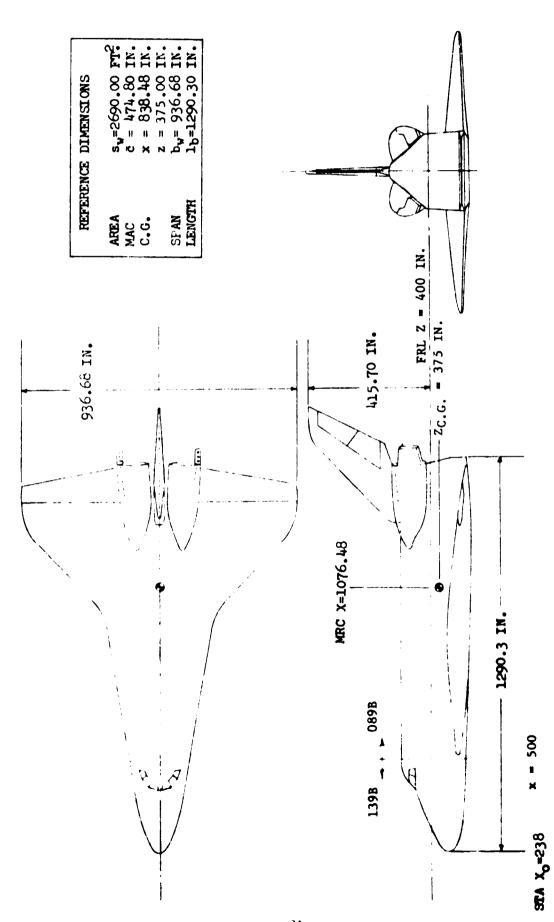
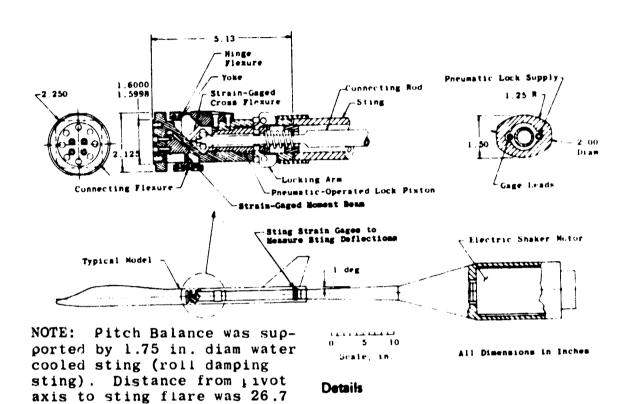
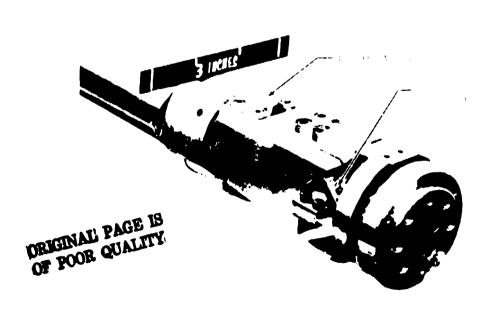


Figure 2. - SSV Orbiter Configuration.



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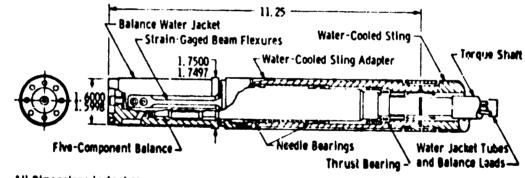
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Photograph of the Balance Assembly VKF 1.B Test Mechanism

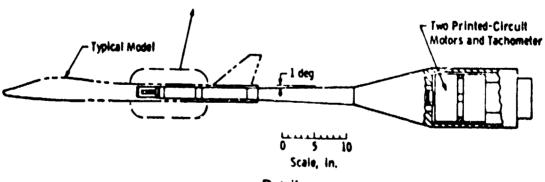
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Figure 3a. Pitch/Yaw Balance Mechanism

Balance	Normal	Pitching	Side	Yawing	Rolling
	Force	Moment	Force	Moment	Moment
-59	500 lb	1125 inlb	40 lb	84 inlb	10 inlb
- 60	1200 lb	2700 inlb	100 lb	210 inlb	100 inlb



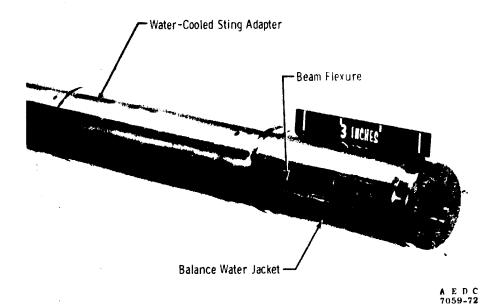
All Dimensions in Inches



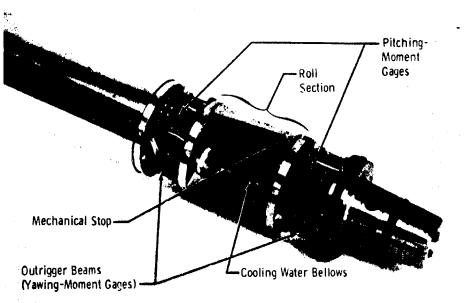
Details
Test Mechanism

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Figure 3b. Roll Balance Mechanism



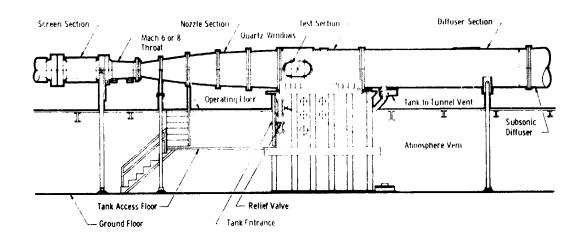
Photograph of the Flexures and Water Jacket



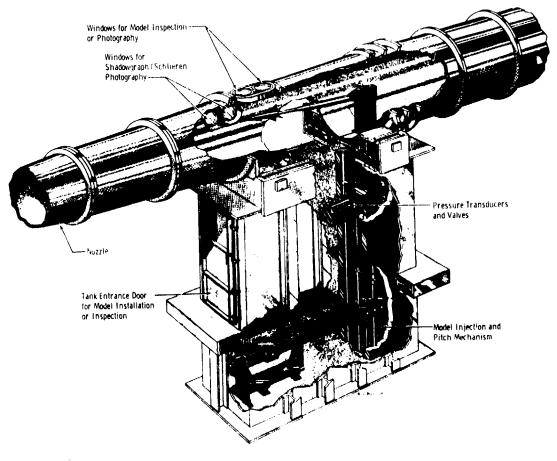
A E D C 8335-72

Photograph of the Balance

Figure 3c. Photograph of Roll Mechanism



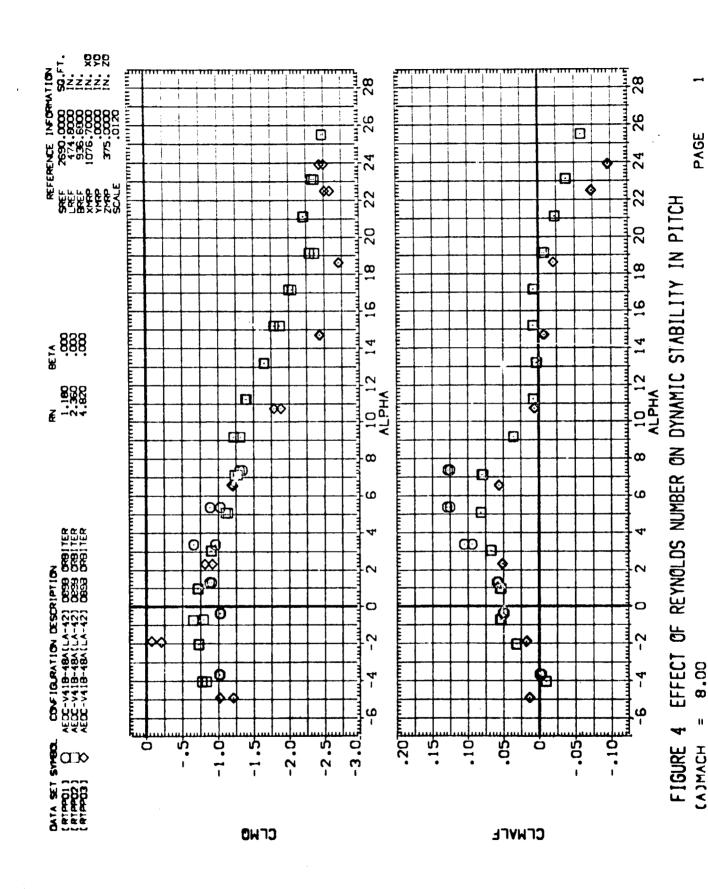
a. Tunnel Assembly



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b. Tunnel Test Section
Tunnel B

DATA FIGURES



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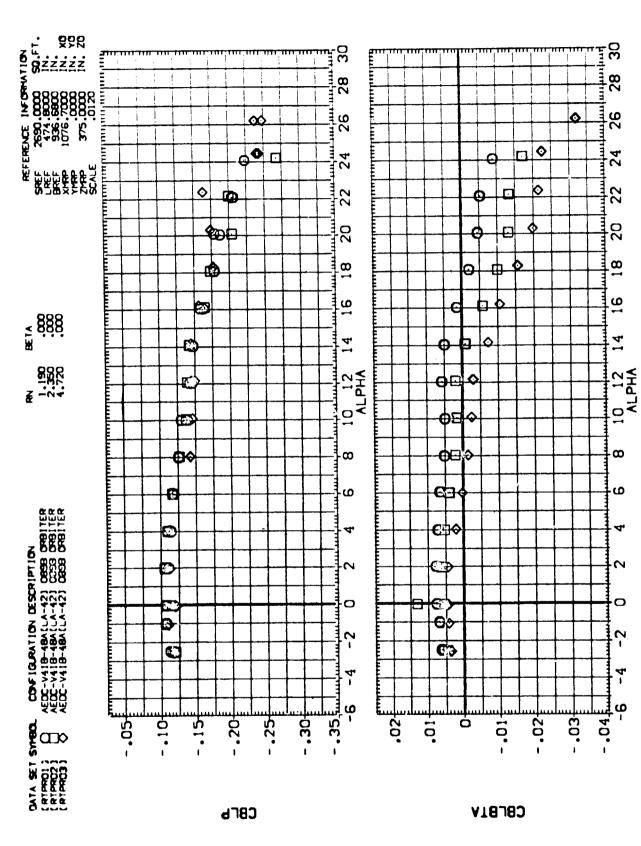
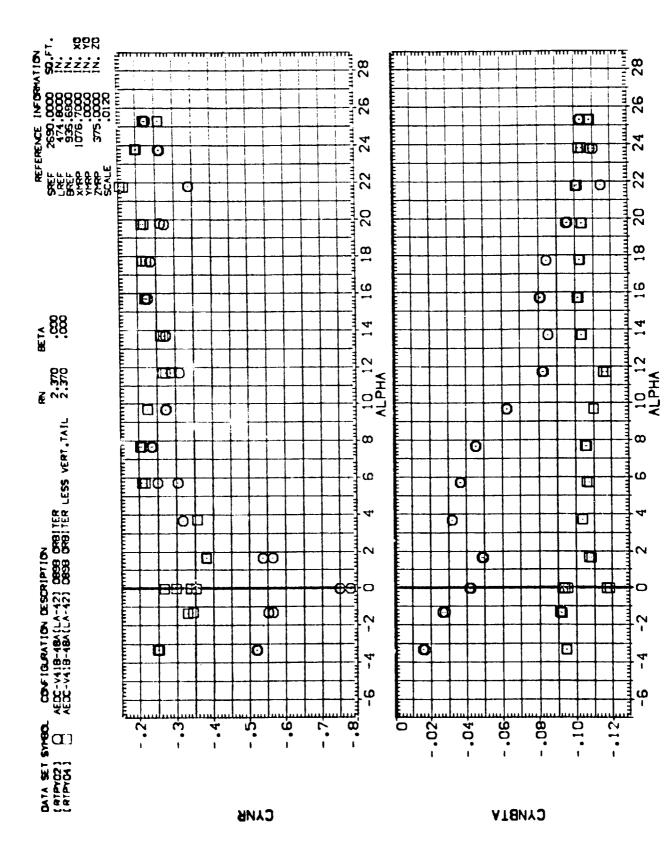


FIGURE S EFFECT OF REYNOLDS NUMBER ON DYNAMIC STABILITY IN ROLL CAJMACH

2

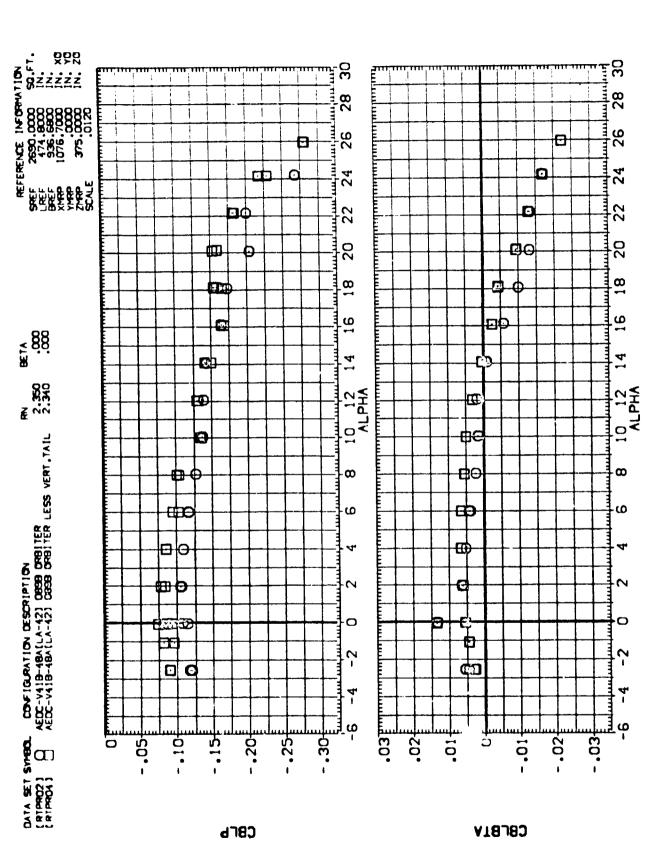
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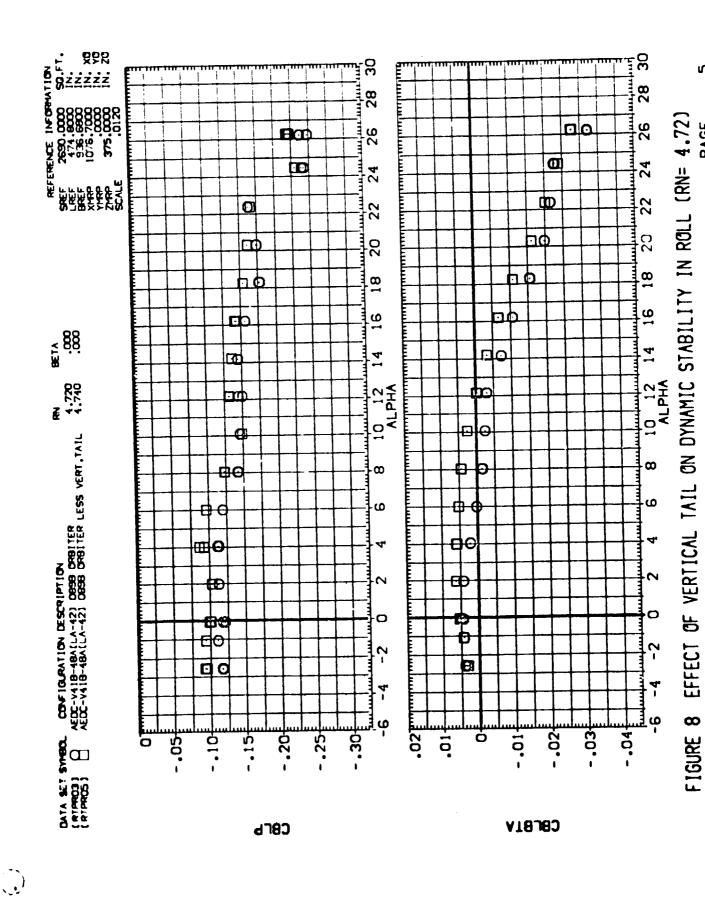
EFFECT OF VERTICAL TAIL ON DYNAMIC STABIL!TY IN YAW 8.00 FIGURE 6 CAJMACH

PAGE

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EFFECT OF VERTICAL TAIL ON DYNAMIC STABILITY IN ROLL (RN= 2.34) 7.38 FIGURE 7 CAJMACH



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CAJMACH =

APPENDIX

TABULATED SOURCE DATA

Tabulations of plotted data are available on request from Data Management Services.

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-.00231

-.00187 -.00195

-.01308

-.00223

-.01067

-.02493

.32479 .32479 .37429

-4.51526 -2.85534

-.04762 .11290 .27820

-4.16334 -4.01780

-.21246 -.25912 -.22301 -.20022

-.01991

-.00210 -.00215 -.00236 -.00239

-.01246 -.01186

-.01259

-.02003 -.02010

.44290 44330 .5154U .516UU .59U7U

-5.31789 -4.68296

-5.62661 -4.97734 -4.62003

-.27498

-,03935

71000.

-.02190

-.00254 -.03276 -. DU277

-.00266

-.01191

-.02188 -.02422 .00071

-.00144

72100.--.03144 -.03159 -.00177

-.00271 -.00274 -.00276

-.03443

-.03528 -.90537

-.02123

0.6601.

-2.37546

-2.48839

-.06324

-2.61528

-2.06795

-.04520 -.06415

01070.

-.00281 -.00281

-.00127

-.00083

-.00259 -.00258 -.00262 -.00264 -.00270

-.00241

-.00349

-.02749 -.02748 -.02576 -.02563

.03260. .03290 .0370.

-.60808

-.02050 -.01939 -.06524

-.00056

-.00044

-.00344

-.00237 -.00242 -.00254

.00035

CLM -.03231 -.03227 -.03087

GRADIENT INTERVAL = -5.00/ 5.00

-.00056

-.00129

-.03085 -.03026 -.03023

-.04830 -.04820 -.03349

-1.00889

-.02600

-.04808

-1.34216 -1.09393

-.06339 -.06118 -.07391

-.00219

10650.-

-.03340 -.00220 -.00200

-2.11:387 -.27356 -.03107

-.00107

-.00158

-.00285 -.00278

-, 00639

-.02380

-.00649

-.02375 -.02497 -.02498

.15840 .15850 .21150

-3.77341

.01365 £0.50. -.05545

-3.18953 -2.14119 -4.13936 -3.75560

-. U3137

-.03196

-.0028U -.0027U

-. 93274 -.00223

-.00824

-.00618

-.02583

.26823

-. 172.489

-.0317703213 -.00214 -.00231

1.190

19

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BETA

(RTFR01) (20 MAR 75

AEDC-V418-48A(LA-42) D898 ORBITER

REFERENCE DATA

TABULATED SOURCE DATA - LA42

DATE D4 AFR 75

PARAMETRIC DATA

AEDC-V418-48A (LA-42) D698 ORBITER

(RTFEGZ) (20 MAR 75)

PARAMETRIC DATA .000 RN

2.350

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BETA

REFERENCE DATA

YMRP = 1076. TOOD IN. YO YMRP = 00000 IN. YO ZMRP = 375.0000 IN. ZO 3AEF = 2690.0000 30.FT.) LREF = 474.8000 IN. 1 DREF = 936.5800 IN. 2 SCALE = .0120 RUN NO. 263/ 0 RIVL = 2.34 GRADIENT INTERVAL = -5.00/ 5.00

5	AFTA		CBLBTA	CTING	Ç	ક	3	Շ	CAN	æ
7.900	-2.550	11962	.00455	.04096	1.90588	07520	03309	51100	00172	00007
7.960	-2.559		.03573	.04142	1.85127	97560	03297	51000.	00193	00009
7.943	043	11456	.00566	00037	84230	03010	03104	00120	00188	00042
7.963	1.473	19450	.00599	01978	-1.24022	00550	02947	00219	00199	00367
7.900	1.96.1	10569	.03652	02444	-1.27616	00660	02942	00255	00209	00067
7.960	3.993	£1601	.00522	01310	-1.47424	.02940	02764	-,00329	002005	00094
7.963	6.010	11691	.00378	00154	-2.14957	.05610	02560	03378	20200	00113
7,983	6.010	11697	.03409	93214	-2.15988	.05640	32558	03392	00206	00113
7.930	6.030	12506	.03222	.04109	-1.28142	06701.	02398	03447	00200	00129
7.983	10.040	13673	75100.	20860.	-2.75794	.15573	32284	00520	00191	00145
7.963	19.040	13519	.50163	.03756	-2.45435	.15500	02283	00536	00195	00146
7.963	12.050	13800	16100.	03483	-3.59299	01102.	02321	00635	90171	00167
7.363	14.060	:4283	00139	05034	-4.09379	.25800	-,02354	00524	991 TO	00185
7.363	14.050	14179	33388	34339	-3.64568	.25863	02358	03643	93175	93186
7.300	16.110	15502	00579	37348	-3.54352	C6125.	0:116	00630	501 78	9020 3
7.983	18.093	17257	01039	04259	-3.32040	.38473	J2178	00522	00186	00223
7.963	27:12	20423	01323	35313	-4.57185	.45590	72297	00619	33181	00245
7.363	22.:73	20052	01335	34173	-4.67913	. 532' .	02507	00613	00174	00271
7.983	24.130	26759	01711	.01468	-3.27849	.61253	02794	00595	00177	00300
7.963		10739	.01329	67850.	28348	03390	03077	00619	00335	00044
	TABICAR	402001	ניגכנט.	6.5010	55215	.01576	.00081	00062	-,00004	00013

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AEDC-V418-48A(LA-42) D096 CRBITER

(RTPR03) (20 MAR 75)

4.720

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PARAMETRIC DATA BETA CX .NI 0000 IN. X3

CY .NI 0000 IN. X3

E 375.02020 IN. Z3 REFERENCE DATA 2000.0000 30.FT. 474.0030 IN. 936.6003 IN.

ð	4			CAN	ď	8	ð	t	CAN	đ
000.	-2.600			05596	1.30971	97480	03443	.00161	00147	00005
9.000	-2.600	٠		.07334	1.73597	97490	03445	.00103	00136	00006
200.	-1.090	٠		.02803	28447	05220	03424	00017	00148	00030
900.		·		.02635	46920	93679	03290	00114	00147	00045
330	000	•		100201	73679	03700	03279	00140	00155	00045
000.	1.960			65720.	59767	00540	03025	00156	00153	33368
0.00	4.010	-		.05276	52910	Cecyco.	02810	00184	00150	00095
333	4.020			.05055	83577	.03120	02804	03196	00152	00096
300.	6.000			.06399	86874	.06719	02605	03231	03143	03114
4.023	0.030	1416	30153	.12529	44663	01/01.	02288	03264	00127	00132
000	0.060			.14777	25529	.10740	02201	00271	00127	00132
0.00	10.093			.04303	-1.63310	.15690	02169	00291	90111	0215U
000.	12.153			06518	-4.48976	.21460	02200	00303	00097	17100
30.	12.153			08434	-4.99669	.21493	02207	03313	•• ((())	171(0
000.	14.18			09754	-6.55666	C8175.	02250	02305	00092	00186
6.00	16.220			00820	-4.83396	.3365.	02328	00310	00079	03205
0.00	16.290			00269	-5.43089	.43743	32428	03338	1,000	00223
1.30	16.295			53850.	-3.99356	.43763	02429	00315	00073	00223
0.00	23.330			.03749	-6.24119	.48070	02556	00306	03063	00244
0.00	22.370			.13285	-4.59837	.55710	02853	03298	900 40	00267
000.	24.440			. 15561	-3.25688	CCC+3.	03122	00263	99029	03300
6.00	24.440			.14924	-3.76433	.64050	03118	00274	00030	03301
0.00	26.223			.14361	-3.96321	0.6617.	03473	03235	03047	03315
3.000	25.220			76.25	-3.34953	. 72393	03471	00213	03347	00316
	TABICAR				28434	0,000	10100	00346	cerce.	00013

ORIGINAL PAGE IS OF POOR QUALITY

AEDC-V418-46A(LA-42) D696 ORBITER LESS VERT-TAIL

PARAMETRIC DATA

(RTPR04) (20 NAR 75)

8.340 Z 900 BETA YMER = 1076.7000 IN. XO YMER = .0000 IN. YO ZMER = 375.0000 IN. ZO REPERENCE DATA ##EF = \$500,0000 #0.FT. LMEF = 474.0000 IN. BMEF = 936.40.30 IN. BCALE = ...

•	į	8		9	97	3	ğ	t	Š	ਵੱ
5			20000	100	1.39322	06320	04714	00149	00106	00070
2	3	- USAGE	90200		1.14330	06310	04718	00166	00111	17000
	26.3-	2000	6000	10,00	- 46799	04130	04493	03230	00122	0000
	2 5	10190 -	25,000	19520	1.71330	04140	04491	03242	00126	0000
2	20.1-	6660	\$6\$00.	2000	1604%	02573	04334	00275	00135	0006
		20000	ecco.	1166.	44/64	02560	04331	00293	00139	0000
2	0.50	96260	econ.	00710	00000		- 04034	CUVIV.	901.54	03304
7.980	36.1	08306	66\$CC.	01186	77133	0.400	10000	90000	100	A)1(4, -
7.963	1.960	07701	.00635	32761	-1.54656	57750	04032	21600	100.	
7.000	5,970	08497	.00554	00412	-1.41826	5880.	03724	00362	-:00157	0316
-	1	96790	.03661	01672	-1.57313	03870	03717	03369	30100	03123
	3	4011	0.000	.03567	23297	.07550	03444	03392	00157	00139
		48760	0.000	0.0000	-1.42227	02570.	03438	00395	00154	00139
			(2)552	3,614.	-1.96547	.11649	10200-	00419	00156	015
		47(4)	30000		-2.71288	.11653	03199	03433	00157	AS 100
			0.0500	22378	-1.40779	.16210	02974	03511	00145	00166
		(4)56.	.00511	.24667	93036	.16240	32378	03525	00:45	0016
		2000	States	CUACU	-2.73446	.23410	02557	00613	00131	00101
	200.51	- 15 C	Sexue.	.04165	-2.46374	.23440	02563	01900	00135	03181
		21.04.	3773	.03113	-1.49196	.26435	02515	03591	00135	00197
		. 14073	90000°	75700.	-2.60631	.26480	02515	03596	00130	00191
		(44)	01275	02396	-2.85734	.32673	02497	03559	00143	0321
		27.31	(2514)	04360	-3.05136	.3265	02489	00566	00145	00214
	36.0	******	1722.	45070	-3.51724	LS695.	03290	00472	00174	00331
	200	20193	32500	1.7840	-2.96934	(3695)	03280	03476	03175	00331
	3.5	. 23855	P(7.1).	.04691	-2.93262	.6195	02979	00523	DOI 69	9330
		7.41.	10.1697	22.520	-3.72733	.61973	87620. −	00529	00190	0330
		*****	96210	28200.	-3.64966	54300	02719	00571	00202	00277
		60101	26210	18600.	-3.61949	. \$4290	02720	00573	0200-	00276
		6081	03969	93160.	-2.99243	.47103	02569	05601	00214	0325
		9181	03949	\$5000.	-3.62475	527	02569	00611	00212	0025
			-, 32444	00219	-2.45416	UT 888.	02501	00662	00214	0323
		15179	00435	36478	-3.49542	39985	02506	00661	00215	00232
	2	VE 28.1.	03445	01366	-2.69503	.39663	02507	00667	03213	03232
		7675	00440	03994	-3.01754	.39610	02507	03672	00212	00231
		07414	.01345	02010.	22322	02320	04268	00074	03265	0008
		25.24	98810	39760.	1.03244	02320	04275	03875	00264	00066
2										



TABLEATED SCHOOL DATA - LA42 DATE 94 AFR 79

AEDC-V418-44A(LA-42) D098 CRBITER LESS VERT.TAIL

(RTFROS) (20 NAM: 75)

PARMETRIC DATA .000

355

4.740

META

ON .NE 0000.376 = 1076.7000 IN. TO THE TABLE TABLE TABLE TO THE TABLE T MAC = 2006.0000 80.FT. LACT = 474.0000 IN. MAC = 936.0000 IN. MALE = .0120

AUTHORE DATA

MUN NO. 201/ U RAVL = 4.72 GRADIENT INTERVAL = -5.00/ 5.00

	2	5	GUBTA	ķ	È	3	ð	Շ	ž	đ
			167140	25 CCU.	1.66227	06640	04763	00304	001 XE	00075
3						06650	04782	00316	00134	00075
95.	2					00000	70170	00365	00137	0006
9.000	-1.070	-03364	.00445	000	ECCC*.	1		10110		PETET -
000.	50	09664	75200.	00110		02910	0440		100	
500	000	100384	95500.	01611	49169	92910	04405	00423	00147	0203
	•	44601	76900	12820	06629	נצונה.	04007	00376	00156	00109
		47.00	100	10350	19051.	.03560	03666	00148	0015	00131
			.00607	.01625	41677	.03600	03662	00391	00160	00131
		AL 300	200	102994	74354	092.6	03392	00400	00151	00147
		12413	03444	.11481	.37519	.11100	02967	03426	(001.36	92165
		W. C	137451	.1:0916	.28224	.11210	32305	00432		00165
		2377	25.00	10609	.14935	.16190	02790	03426	00126	00.78
	200	7 (A)	033X	06121	-3.35174	667.15.	02737	03396	90121	00195
		\$126.	0x22	87850	-3.19294	.2175.)	02705	00404	15 (00:-	00195
		13921	W. C.	06337	-3.65734	.27643	02654	03363	00116	00210
		91171	1,07673	7.970	-4.26359	29:	32643	03325	11100	00224
	200		- 77664	16750	-4.04114	CCESS.	02642	00331	03113	0322
		4977	- 01000	£8610	-4.79699	.40520	02676	02294	00112	03234
		With	0.2910 -	03473	-7.31995	.47955	32755	-,03250	00108	03260
		16709		C2221.	-2.97710	65780	02936	03221	03095	3328.
	74.46	14146		.12147	-2.34962	.63 8 00	03211	00163	00041	0030
		*1646	- 112 YBA	71031.	-3.36.36	67,17.	03542	03123	84000	0333
		16016	2777	.14951	-3.25,441	.71850	03544	00128	-, 00000	.0333
	26.240	11262	02772	15991	-2.41863	.71320	03546	00134	00381	33
	94.94	22319	02773	15932	-2.69283	41.933	03545	00135	00381	0033
}		2000	17.774.0	33.66	23156	61510	67100	0,000,-	-,00004	

ORIGORGE IE ORIGINATION OF PINCE CONTINUE

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(D6 NOV 74

PARAMETRIC DATA

1.180

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BETA

AEDC-V418-48A(LA-42) D898 ORBITER

(RTPPD1)

REPERENCE DATA

= 1076.7000 IN. XO = .0000 IN. YO = 375.0000 IN. ZO XX XX Y 2690.0000 30.FT. 474.9000 IN. 936.6800 IN.

LREF = SCALE =

GRADIENT INTERVAL = +5.007 5.00 RVL " . V **35. 35. 35.**

-.02610 -.02610 .00063 -.02940 -.02940 -.02770 CLM
-.03370
-.03370
-.03230
-.03220
-.03050 -.02773 CLMALF
-.00290
-.00160
.04950
.05760
.05780
.05980
.05980 .12540 .12490 .12870 CLN0
-1.02200
-1.02200
-1.02700
-1.02100
-.90300
-.95900 -1.33900 -1.30100 -1.03073 -1.03300 -.889DD ALFHA
-3.670
-3.670
-.370
-.370
1.330
1.320
3.350
3.350
5.380
7.400
7.400 6.000 6.000 6.000 8.000 8.000 8.000 8.000 6.000 6.000 8.000 8.000

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(RTFF02) (06 NOV 74)

PARAMETRIC DATA

2.360

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BETA

REFERENCE DATA

= 1076. TOOD IN. YO = .0300 IN. YO = 375.0000 IN. ZO XIARP YHARP ZHARP = 2690.0000 30.FT. = 474.8000 IN. 936.6800 IN. LAEF ...

GRADIENT INTERVAL = -5.00/ 5.00 = 1.83 ₹ ₹ 0 /92 RUN KO

-.03080 -.03480 .00053 -.02370 -.02370 -.02450 -.02679 -.02989 -.02789 -.02579 -.02579 -.02320 -.02450 -.02540 -.02540 -.02660 -.02840 -.03080 CLM -.03340 -.03320 -.03320 -.03240 -.03130 -.03130 -.0238 -.02370 -.03240 -.00800 -.00530 -.02300 -.03839 .00570 CLMALF -.01000 -.00910 .03110 .03530 .03520 .07700 .00190 .00730 .00680 .02730 02700. -.03880 .05330 .05300 .06729 .05810 .08130 .08140 .07860 .07990 .05483 -1.40299 -1.38999 -1.64593 -2.04300 -2.36300 -2.33800 -1.22600 -1.31000 -1.21900 -1.1960 -1.1360 CLM2 -.83390 -.77199 -.71800 -.90500 -1.87900 -2.00400 -2.29300 -2.21600 -2.22100 -2.37000 -. 71399 -. 78600 -1.27500 -1.65733 CC967.1--.64800 -. 73599 **-.89**000 -. 73990 21.130 23.190 13.200 15.200 17.160 17.171 19.160 19.160 21.130 .980 .980 3.040 3.040 5.070 7.140 7.140 9.160 9.170 11.210 13.200 15.210 23.100 ALPHA -4.050 -4.050 -2.050 -2.060 -.7211 7.950 7.950 7.950 7.950 7.950 7.950 7.950 7.950 7.950 7.950 7.950 7.95U 7.95U 7.95U 7.950 7.950 7.95U 7.950 7.950 7.950 7.95 7.950 7.950 7.950 7.950 7.950 7.950 7.950

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SCALE =

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(RTPPG3) (06 NOV 74)

PARAMETRIC DATA .000 RN

4.820

BETA =

REFERENCE DATA

SAEF = 2690.0000 30.FT. XMRP = 1076.7000 IN. XO LAEF = 474.6000 IN. YMRP = .0000 IN. YO BREF = 936.6600 IN. ZMRP = 375.0000 IN. ZO SCALE = .0120

RUN NO. 61/ 0 RN/L = 3.73 GRADIENT INTERVAL = -5.00/ 5.00

CLM 03520 03520	03490	03030 02590 02580	02360 02360 02480	02480 02700 03110	03110 03370 033370
CLMALF .01290	01710. 03710. 03130.	.05220. .05600. 05670.	.00520 .00570 .00570	02690 02090 07430	07340 09750 09740
CLM3 -1.02400 -1.20300	07000	919DU -1.2D7DU -1.188DU	-1.78800 -1.88400 -2.43400	-2.44000 -2.71700 -2.51400	-2.58900 -2.50100 -2.44300
ALPHA -4.910 -4.910	-1.890	2.330 6.560 6.570	10.710	14.700 18.630 22.500	22.500 23.900 23.900 68.401 EV.
MACH 8.000	8 9 90 000 8	8.000 8.000	8.000 8.000	8.000 8.000 8.000	8.000 8.000 8.000

(D6 NOV 74

(RTFYD2)

PARAMETRIC DATA

2.370

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BETA

REFERENCE DATA

AEDC-V418-48A(LA-42) 0698 ORBITER

ZHRF X X Y z 2690.0000 39.FT. = 474.8000 IN. z 936.6600 IN. E z .0120

GRADIENT INTERVAL = -5.00/ 5.00 RN/L = 1.82 0 /00 SCN NO.

-.00123 -,00030 -,00030 -,00040 0€000.-0€0000:--.00120 01000.--.00060 -.00060 -,00120 -.00120 .03020 .03000 01000 00000. 00000. 00000. 06000.-.00030 05000. .00040 -.19439 -.19439 -.11519 -.ce500 -.ce600 -.08260 -.0264U -.028UU -.0416U -.04240 -.03189 -.04570 -.0812 -.08153 C6260,--.10940 -.11093 CYNBTA -.0158U -.0166U -.08340 -.ധിഡോ -.05270 -.05290 -.04880 ~.04950 -.03710 -.04520 -.22500 -.22600 -.23500 -.25200 -.25103 -.33900 -.53800 CYNR -.51800 -.52100 -.56409 -.55300 -.23300 ..275.-00275.--.25300 -.22400 UC755.--.75000 -.23600 -,31009 -.28833 -.27500 C.C.572.--.31600 -.30400 -.250:30 13.710 15.720 15.720 17.720 19.720 19.750 23.750 25.230 21.703 GRADIE4T 7.68U 3.690 11.680 1.660 1.660 3.640 5.710 5.710 089.7 9.593 25.293 ALFHA -3.340 -3.340 -1.340 -1.340 -.040 040.-6.000 8.000 6.000 6.000 6.000 6.000 6.000 6.000 6.000 6.000 8.000 8.000 8.000 6.000 8.000 8.000 8.000 8.000 8.000 8.000 8.000 6.000 8.000 8.000

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34, 3

LREF = BREF = SCALE =

AEDC-V418-48A(LA-42) 0898 ORBITER LESS VERT.TAIL

(RIPYD4) (06 NOV 74)

PARAMETRIC DATA

2.370

.000 RN

BETA

XMRP = 1076.7000 IN. XO YMRP = .0000 IN. YO ZMRP = 375.0001 IN. ZO BAEF = 2000.0000 50.FT. LREF = 474.0000 IN. BAEF = 936.6000 IN. SCALE = .0120

REFERENCE DATA

RUN NO. 112/ D RIVL = 1.83 GRADIENT INTERVAL = -5.00/ 5.00

MAGM	ALPHA	CYNE	CYNBTA	S S
9.000	-3.350	25200	09490	000 7 0
8.000	-3.350	24709	09520	0.000
6.000	-1.330	34300	09180	0.000
8.000	-1.350	32800	09240	00070
6.000	040	2980	09280	<u>07000-</u>
6.000	050	26500	09410	00070
6.003	050	35200	09610	6,000
6.000	1.650	38100	10770	00060
8.000	1.650	37900	10870	-,00060
600.8	3.700	35500	10420	00060
6.000	5,733	21500	10690	00060
8 .000	5.710	20803	10790	00060
6.000	7.69	20300	10613	00000
6.000	7.69	20800	19700	00060
8.000	9.690	22403	11050	00060
6.003	11.710	25700	11590	00060
8.500	11.710	27300	11750	- .9998 0
8.000	13.710	25900	10379	00060
6.000	13.710	26900	10440	00060
8.000	15.730	22100	10190	0.7000
8.000	15.730	22100	10270	07000
8.000	17.763	22500	10300	00080
0.000	17.760	21400	10360	0000
6.000	19.730	21100	10410	000380
6.000	19.733	21833	10460	.00000
8.000	21.75	16300	10150	.ecco
6.000	21.760	15400	10230	-,000000
6.000	23.790	19800	10320	00110
6.000	23.790	20100	10483	00110
8.000	25.28	26333	10880	00120
8.000	25.283	22133	10940	US100
8.000	050	33739	11730	-,000090
6.000	040	33800	11883	00090
	CRADIENT	01707	00207	50000